



Novel solution for heat and mass transfer of a MHD micropolar fluid flow on a moving plate with suction and injection

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Abstract

Two new functions on the semi-infinite interval, namely Rational Gegenbauer (R) and Exponential Gegenbauer (E) functions are proposed to solve the heat transfer problem. The considered problem is flow of MHD micropolar over a moving plate with suction and injection boundary conditions. For applying Tau method efficiently, two matrices of derivative and product for both of rational and exponential Gegenbauer whose enable us to solve a system of nonlinear algebraic equations on the semi-infinite interval were introduced, and an error bound of these functions approximation was estimated which led to have an exponential convergence rate in this method. Moreover, the influence of the important physical parameters on heat and mass transfer phenomena are studied with details. Comparing the results of Rational Gegenbauer Tau and Exponential Gegenbauer Tau methods with available analytical and numerical solutions shows that the present methods are efficient and have fast convergence rate and high accuracy. This method can solve a set of coupled nonlinear and high-order differential equations on a semi-infinite domain by converting to a set of linear equations.

Keywords Tau method · Rational Gegenbauer functions · Exponential Gegenbauer functions · Magneto-micropolar · Suction and injection · Radiation heat transfer

Mathematics Subject Classification 34B15 · 34B40 · 65L05 · 65L60

List of symbols

b Constant
 B_0 Uniform transverse magnetic field

c_f Skin-friction coefficient
 c_p Specific heat at constant pressure
 Ec Eckert number
 f Dimensionless velocity
 G Microrotation parameter
 g Dimensionless microrotation
 G_1 Microrotation constant
 K Coupling constant parameter
 k^* Mean absorption coefficient
 M Magnetic field parameter
 N Components of microrotation
 Nu Nusselt number
 Pr Prandtl number
 q_r Radiative heat flux
 q_w Surface heat flux
 R Thermal radiation parameter
 Re Reynolds number
 s Constant characteristic of the fluid
 T Temperature of fluid
 u, v Velocity components along x and y directions, respectively

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x, y Cartesian coordinates along the plate and normal to it, respectively

Greek symbols

η	Similarity variable
γ	Constant
κ	Thermal conductivity
μ	Dynamic viscosity
ν	Kinematic viscosity
ρ	Density of the fluid
σ	Electrical conductivity
σ^*	Stefan–Boltzmann
τ	Skin friction
θ	Dimensionless temperature
φ	Stream function

Subscript

∞	Ambient condition
w	Condition of the wall

1 Introduction

Spectral methods are developing very fast for solving ordinary and partial differential equations [1–4]. Their superior rate of convergence for sufficiently smooth functions seems to be their main appeal. One of the most popular methods of classical spectral category is Tau method which is an approximation technique introduced by Lanczos [5] and used to solve differential equations. The main idea of this approach is implementing a set of orthogonal functions for expanding a function that obtains an approximate solution without demanding to satisfy the boundary conditions by the expansion functions [6–9].

Many problems in science and engineering can be modelled by partial/ordinary differential equations in unbounded/semi-infinite/finite domains, and spectral methods are a promising tool for solving such problems. One direct approach for numerical simulation is using the orthogonal polynomials over unbounded domains, by spectral methods [10–13]. For instance, the Laguerre and Hermite polynomials can be considered in this category. Other approaches like Chebyshev and Jacobi polynomials can be used in bounded domains, but for implementing them, a preprocessing is need that can be satisfied by mapping the original problem in infinite domain to a finite domain [14, 15]. Moreover, the domain truncation method can be used which in, the infinite intervals are replaced by sufficiently large intervals [16]. Using the technique based on the rational approximations is another approach that introduced for the first time by Christov [17] and Boyd [18,

19]. The rational Chebyshev functions defined in [18] and afterward Guo et al. [20] applied the rational Legendre functions as a new set of functions in a spectral method. These two functions are mutually orthogonal on the semi-infinite domain. Therefore, subsequent research was shifted towards solving the nonlinear ordinary differential equations on semi-infinite intervals by applying these rational functions in spectral methods such as collocation and Tau approach based on operational matrix [21–30].

In this paper, we focus on one of the most important orthogonal polynomials, namely Gegenbauer polynomials which are a general case of Chebyshev and Legendre polynomials and make rational Gegenbauer and exponential Gegenbauer functions for solving the systems of nonlinear ordinary differential equations (ODEs) Navier–Stokes equations for micropolar fluids, on a semi-infinite domain. Indeed, the superiority of the rational and exponential Gegenbauer functions for satisfying the boundary conditions defined on a semi-infinite domain than the polynomials basis, appears in solving this type of fluid problem. We use Tau method to solve this problem and present the operational matrices of derivative and product of rational and exponential functions to reduce the solution of this problem to the solution of a system of nonlinear algebraic equations. Also, we analyze the error of function approximation of the method by these types of basis functions which deduces that approximation of the function defined in $[0, \infty)$ is exponential convergence.

In recent years, researchers have become more interested in micropolar fluids flow (a subclass of microfluids) because they are widely used in many applications in industry and science [31, 32]. The theory of micropolar fluids was first introduced by Eringen [33, 34]. This theory demonstrates the effects of local rotary inertia and coupled stresses. Also, it can describe flow behaviour, while classical Newtonian fluid theory is not enough. Łukaszewicz [35] gave comprehensive reviews for both of theory and applications of this research topic in his book. Also, one can refer to [36] for more detail of applications of the micropolar fluids.

The surfaces which in polymer sheets or filaments continuously drawn from a die are denoted by continuous surfaces. The concept of continuous surfaces been proposed by Sakiadis [37]. The boundary layer flow on continuous surfaces is one of the important flow and it appear in some technical operations. Soundalgekar and Takhar investigated the flow and heat transfer past a continuously moving flat plate in a micropolar fluid [38].

With the emergence of the problem of stretching sheet in engineering, Crane [39] was the first researcher who studied the flow generated due to an elastic sheet and the velocity of it is changed linearly according to the distance that measured from a fixed point on the surface.

Afterwards, subsequent researchers interested in research on stretching sheet and obtained some good results [40, 41]. Chamkha et al. [42] investigated the effects of chemical reaction on unsteady free convective heat and mass transfer on a stretching surface in a porous medium. Ress and Bassom [43] studied the Blasius boundary-layer flow of a micropolar fluid over a flat plate. The subject of heat and mass transfer on a stretching sheet with suction or injection was studied well in [44]. The numerical and approximation methods were investigated for the problem of micropolar fluid from a non-isothermal stretching sheet by considering the concepts of suction and injection in [45] and [46], respectively. Also, the presence of radiation was considered in [47, 48] and they investigated the heat transfer of a micropolar and the flow of a micropolar fluid past a continuously moving, respectively. Damseh et al. [32] considered the problem of combined heat and mass transfer by natural convection of a micropolar, viscous and heat generating or absorbing fluid flow near a continuously moving vertical permeable infinitely long surface in the presence of a first-order chemical reaction. Numerical and analytical solutions of the developing laminar free convection of a micropolar fluid in a vertical parallel plate channel with asymmetric heating were studied in [49]. Rahman et al. [50] studied the two-dimensional steady boundary layer equations for hydro-magnetic convective heat transfer flow of micropolar fluid flowing along a heated inclined flat plate with variable electric conductivity and uniform surface heat flux in the presence of non-uniform heat source or sink. Moreover, in some research, the dependence and influence of another and different parameters on micropolar fluid have been studied [31, 51].

Magnetohydrodynamic (MHD) flows also arise in many applications and several researchers reported studies on MHD-free convection and mass transfer flows [52, 53]. Takhar et al. [54] presented analysis deals with the unsteady flow and heat transfer over a semi-infinite flat plate with an aligned magnetic field and considered plate is impulsively moved with a constant velocity. The presence of heat generation or absorption, and suction or injection effects on steady natural convection boundary-layer flow of a nanofluid was considered in [55]. Seddeek [56] considered the flow of a magneto-micropolar fluid past a continuously moving plate and studied the effect of radiation on the flow of this fluid with suction and blowing in [57]. Moreover, in [58], the MHD micropolar fluid past a stretched permeable surface with heat generation or absorption was studied. Joule heating, chemical reaction and radiation effects on a MHD micropolar fluid were also considered in [59]. Bhargava et al. [60] studied a two-dimensional fully developed steady-state, viscous hydrodynamic flow of a deoxygenated biomagnetic micropolar fluid by finite element method. Recently, Aslani et al. [61] considered the

micromagnetorotation (MMR) effect in micropolar MHD flows, by assuming that magnetization and magnetic field vectors are parallel which is applicable in industrial and bioengineering.

Sometimes, the governing nonlinear equations that describe these problems do not have the exact solutions and the solution that comes to mind is using numerical to solve these nonlinear equations [62, 63]. So, the objective of this paper is to investigate the numerical method for equations about the flow of magneto-micropolar fluid by considering radiation and study the effect of different parameters on some important flow characteristics.

The paper continues as follows: In the next section, the set of equations for the problem that is derived from mathematical relationships is described. Sections 3 and 4 review some favourable properties of the rational Gegenbauer functions and exponential Gegenbauer functions, respectively. The convergence rate of these functions approximation is discussed in Sect. 5. In Sect. 6, we use each of these two functions as basis functions in Tau method to solve a system of nonlinear ODEs on the semi-infinite interval and present some numerical results which ensure the accuracy of our method in Sect. 7. Section 8 concludes the paper with a brief summary.

2 Formulation of the problem

The steady, laminar, incompressible, viscous, micropolar and electrically conducting fluid flowing past a continuously moving plate with a constant velocity is assumed [57]. Here, we assumed there is no electric field and the Hall effect of magnetohydrodynamics is neglected. According to [57], the governing equations within boundary layer approximation can be written as

$$\begin{aligned} \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} &= 0, \\ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} &= \nu \frac{\partial^2 u}{\partial y^2} + k_1 \frac{\partial N}{\partial y} - \frac{\sigma B_0^2}{\rho_\infty} u, \\ G_1 \frac{\partial^2 N}{\partial^2 y} - 2N - \frac{\partial u}{\partial y} &= 0, \\ u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} &= \frac{\kappa}{\rho c_p} \frac{\partial^2 T}{\partial y^2} - \frac{1}{\rho c_p} \frac{\partial q_r}{\partial y} + \frac{\nu}{c_p} \left(\frac{\partial u}{\partial y} \right)^2, \end{aligned} \quad (1)$$

with below boundary conditions

$$\begin{aligned} u &= bx, \quad v = v_w, \quad N = 0, \quad T = T_w, \quad \text{at } y = 0, \\ u &\rightarrow 0, \quad N \rightarrow 0, \quad T \rightarrow T_\infty, \quad \text{at } y \rightarrow \infty. \end{aligned} \quad (2)$$

Here u and v are the velocity components along the flow direction (x -direction) and normal to flow direction (y -direction), ν is the kinematic viscosity, N is the components

of microrotation or angular velocity, σ is the electrical conductivity and B_0 is a uniform strong magnetic field in the y -direction. In addition, $k_1 = \frac{s}{\rho}$ is the coupling constant that s is a constant characteristic of the fluid and ρ is the density. G_1 is the microrotation constant, T is the fluid temperature, κ is the thermal conductivity, c_p is the specific heat of the fluid at a constant pressure and q_r is the radiative heat flux.

In boundary conditions, T_w is a constant temperature of the wall, T_∞ is a constant temperature of ambient fluid ($T_\infty > T_w$) and b is constant.

By the Rosseland approximation [64], the radiative heat flux is written as

$$q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial T^4}{\partial y}, \quad (3)$$

where σ^* and k^* are the Stefan-Boltzmann constant and the mean absorption coefficient, respectively. By assumption that the temperature differs in the flow, can expand the term T^4 in a Taylor series about T_∞ and by overlooking the higher-order parts, we have

$$T^4 \simeq 4T_\infty^3 T - 3T_\infty^4. \quad (4)$$

Now, under consideration of the following similarity variables, the governing partial differential equations can convert to a system of coupled nonlinear ordinary differential equation (ODEs)

$$\begin{aligned} \eta &= b^{1/2} v^{-1/2} y, & \varphi &= (bv)^{1/2} x f(\eta), \\ N &= b^{3/2} v^{-1/2} x g(\eta), & \theta(\eta) &= \frac{T - T_\infty}{T_w - T_\infty}, \end{aligned} \quad (5)$$

where $\varphi(x, y)$ is a stream function such that $u = \frac{\partial \varphi}{\partial y}$ and $v = -\frac{\partial \varphi}{\partial x}$.

So, from the above equations, the transformed equations as systems of nonlinear ordinary differential equation are [57]:

$$\begin{aligned} f''' + ff'' - (f')^2 - Mf' + Kg' &= 0, \\ Gg'' - (2g + f'') &= 0, \\ \left(\frac{1+R}{RPr}\right) \theta'' + f\theta' - \gamma f'\theta + Ec(f'')^2 &= 0, \end{aligned} \quad (6)$$

and the boundary conditions on a semi-infinite computational domain as follow:

$$\begin{aligned} f(0) &= f_w, & f'(0) &= 1, & f'(\infty) &= 0, \\ g(0) &= 0, & g(\infty) &= 0, \\ \theta(0) &= 1, & \theta(\infty) &= 0, \end{aligned} \quad (7)$$

where f , g and θ are similarity functions for velocity, microrotation and temperature, respectively and their derivatives are respect to η (similarity variables), γ is a

constant parameter. The important physical parameters are as follow:

$$\begin{aligned} Pr &= \frac{\rho c_p \nu}{K}, & M &= \frac{\sigma B_0^2}{\rho_\infty B}, \\ R &= \frac{3Kk^*}{16\sigma^* T_\infty^3}, & K &= \frac{k_1}{\nu}, \\ G &= \frac{G_1 B}{\nu}, & Ec &= \frac{u_w^2}{c_p (T_w - T_\infty)}, \end{aligned} \quad (8)$$

that they are the Prandtl number, magnetic field parameter, radiation parameter, coupling constant parameter, microrotation number and Eckert number, respectively.

For the suction and injection case f_w is positive, negative, respectively. The skin friction of the considered surface can be obtained as [45]:

$$\tau_w = -\mu_w (u_w)^{3/2} (vx)^{-1/2} f''(0). \quad (9)$$

With considering $Re = \frac{u_w x}{\nu}$ as the Reynolds number, the friction coefficient (c_f), heat flux (q_w) and Nusselt number (Nu) are as follow:

$$\begin{aligned} c_f &= -(Re)^{-1/2} f''(0) \\ q_w &= -K(T_w - T_\infty) (u_w)^{1/2} (vx)^{-1/2} \theta'(0), \\ Nu &= -(Re)^{1/2} \theta'(0). \end{aligned} \quad (10)$$

3 Rational Gegenbauer functions

In this section, the definition of rational Gegenbauer functions and their properties will be presented. Let n be an integer variable, the Gegenbauer polynomials of degree n are defined as follow [65]:

$$\begin{aligned} G_n^\alpha(t) &= \sum_{j=0}^{[n/2]} (-1)^j \frac{\Gamma(n+\alpha-j)}{j!(n-2j)!\Gamma(\alpha)} (2t)^{n-2j} \quad \text{for } \alpha > -\frac{1}{2}, \end{aligned} \quad (11)$$

where Γ is the Gamma function.

These polynomials are orthogonal in $[-1, 1]$, with the following weight function $\rho(t) = (1-t^2)^{\alpha-1/2}$, for a fixed value of α , G_n^α can be obtained as [66]:

$$\begin{cases} G_0^\alpha(t) = 1, \\ G_1^\alpha(t) = 2\alpha t, \\ G_{n+1}^\alpha(t) = \frac{1}{n+1} [2y(n+\alpha)G_n^\alpha(t) - (n+2\alpha-1)G_{n-1}^\alpha(t)], \quad n \geq 1. \end{cases} \quad (12)$$

With considering the new basis functions according to the Gegenbauer polynomials and call them rational

Gegenbauer functions as $R_n^\alpha(x) = G_n^\alpha(\frac{x-L}{x+L})$, where $\alpha > -\frac{1}{2}$ and L is a constant parameter, which one can properly choose it to adjust the length of the desired interval [67]. The following recursive formulas for $R_n^\alpha(x)$ can be derived easily:

$$\begin{cases} R_0^\alpha(x) = 1, \\ R_1^\alpha(x) = 2\alpha \frac{x-L}{x+L}, \\ R_{n+1}^\alpha(x) = \frac{1}{n+1} \left[2 \left(\frac{x-L}{x+L} \right) (n+\alpha) R_n^\alpha(x) - (n+2\alpha-1) R_{n-1}^\alpha(x) \right], n \geq 1. \end{cases} \quad (13)$$

It should be mentioned that the weight function is: $w_r^\alpha(x) = \frac{2L}{(x+L)^2} \left[1 - \left(\frac{x-L}{x+L} \right)^2 \right]^{\alpha-\frac{1}{2}}$, and the orthogonality the interval is a semi-infinite domain as: $[0, \infty)$. The following integral formula can be considered for the orthogonal functions:

$$\int_0^\infty R_n^\alpha(x) R_m^\alpha(x) w_r^\alpha(x) dx = \frac{\pi 2^{1-2\alpha} \Gamma(n+2\alpha)}{n!(n+\alpha) \Gamma^2(\alpha)} \delta_{nm}, \quad (14)$$

where δ_{nm} is the Kronecker function. The differentiation formula for Gegenbauer polynomials is [65]:

$$\dot{G}_n^\alpha(t) = \frac{d}{dt} G_n^\alpha(t) = 2\alpha G_{n-1}^{\alpha+1}(t), \quad (15)$$

therefore, the following formula for the derivative can be obtained:

$$\dot{R}_n^\alpha(x) = \frac{d}{dx} R_n^\alpha(x) = \frac{4\alpha L}{(x+L)^2} R_{n-1}^{\alpha+1}(x). \quad (16)$$

With respect to Eqs. (14) and (16), we discover that $\dot{R}_n^\alpha(x)$ are also mutually orthogonal considering the weight function $\widehat{w}_r^\alpha(x) = \frac{(x+L)^2}{8Lx^2} \left[1 - \left(\frac{x-L}{x+L} \right)^2 \right]^{\alpha+\frac{1}{2}}$. Hence

$$\int_0^\infty \dot{R}_n^\alpha(x) \dot{R}_m^\alpha(x) \widehat{w}_r^\alpha(x) dx = \frac{\pi 2^{-(2\alpha+1)} \Gamma(2\alpha+n+1)}{(n-1)!(n+\alpha) \Gamma^2(\alpha+1)} \delta_{nm}. \quad (17)$$

Function approximation An arbitrary function $\varphi(x)$ on the semi-infinite interval $[0, \infty)$ can be expanded with a fixed value of α as:

$$\varphi(x) = \sum_{j=0}^\infty a_j R_j^\alpha(x), \quad (18)$$

where

$$a_j = \frac{j!(j+\alpha) \Gamma^2(\alpha)}{\pi 2^{1-2\alpha} \Gamma(j+2\alpha)} \int_0^\infty R_j^\alpha(x) \varphi(x) w_r^\alpha(x) dx. \quad (19)$$

If $\varphi(x)$ in Eq. (18) is truncated after the N th terms, then

$$\varphi_N(x) = \sum_{j=0}^{N-1} a_j R_j^\alpha(x) = A^T R^\alpha(x), \quad (20)$$

where the entity of A and $R^\alpha(x)$ vectors are listed as unknown coefficients and rational Gegenbauer functions with different degrees:

$$A = [a_0, a_1, \dots, a_{N-1}]^T, \quad (21)$$

$$R^\alpha(x) = [R_0^\alpha(x), R_1^\alpha(x), \dots, R_{N-1}^\alpha(x)]^T. \quad (22)$$

Derivative operational matrix The derivative of the vector $R^\alpha(x)$ [Eq. (22)], is a matrix:

$$\dot{R}^\alpha(x) = \frac{dR^\alpha(x)}{dx} \simeq D_r R^\alpha(x). \quad (23)$$

For obtaining the elements of square matrix $(N \times N)$, the following recursive formula can be implemented:

$$\begin{cases} \dot{R}_0^\alpha(x) = 0, \\ \dot{R}_1^\alpha(x) = \frac{4\alpha L}{(x+L)^2} = \frac{1}{L} \left[\frac{\alpha(3+2\alpha)}{2(\alpha+1)} R_0^\alpha(x) - R_1^\alpha(x) + \frac{1}{2(\alpha+1)} R_2^\alpha(x) \right], \\ \dot{R}_{n+1}^\alpha(x) = \frac{1}{n+1} \left[\left(\frac{n}{\alpha} + 1 \right) \frac{d}{dx} (R_n^\alpha(x) \cdot R_1^\alpha(x)) - (n+2\alpha-1) \dot{R}_{n-1}^\alpha(x) \right], n \geq 1. \end{cases} \quad (24)$$

Therefore one can figure out that D_r , is a lower-Hessenberg matrix and can be defined as $D_r = \frac{D_1 + D_2}{L}$; where D_1 can be formulated by considering all elements of the first row ($i = 0$) are zero and other elements obtained from the following tridiagonal matrix

$$D_1 = \text{diag} \left(\frac{\alpha^2}{\alpha+i} + \frac{3(2i-1)\alpha}{2(\alpha+i)} + \frac{7i(i-1)}{4(\alpha+i)}, \right. \\ \left. -i, \frac{i(i+1)}{4(\alpha+i)} \right), i = 1, \dots, N-1, \quad (25)$$

and the entities of matrix D_2 are determined by $d_{10} = \frac{3}{2}$ if $\alpha = 0$ and the following conditional expression for other elements

$$d_{ij} = \begin{cases} 0, & j \geq i-1, \\ (-1)^{i+j+1} c_{\alpha j}, & j < i-1, \end{cases} \quad (26)$$

where $c_{00} = 2$ and $c_{\alpha j} = 2(\alpha+j)$ for other cases.

According to the previous formula, for a fixed value of $\alpha \neq 0$ and considering $N = 5$, the derivative operational matrix will have the following form:

$$D_r = \frac{1}{L} \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ \frac{\alpha(2\alpha+3)}{2(\alpha+1)} & -1 & \frac{1}{2(\alpha+1)} & 0 & 0 \\ -2\alpha & \frac{(\alpha+1)(2\alpha+7)}{2(\alpha+2)} & -2 & \frac{3}{2(\alpha+2)} & 0 \\ 2\alpha & -2(\alpha+1) & \frac{2\alpha^2+15\alpha+21}{2(\alpha+3)} & -3 & \frac{3}{\alpha+3} \\ -2\alpha & 2(\alpha+1) & -2(\alpha+2) & \frac{2\alpha^2+21\alpha+42}{2(\alpha+4)} & -4 \end{pmatrix}.$$

Moreover, if we consider $\alpha=0$ and $L=1$, the matrix is as follows

$$D_r = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 3/2 & -1 & 1/2 & 0 & 0 \\ -2 & 7/4 & -2 & 3/4 & 0 \\ 2 & -3 & 7/2 & -3 & 1 \\ -2 & 3 & -5 & 21/4 & -4 \end{pmatrix}.$$

Product operational matrix In producing the two rational Gegenbauer function vectors we have the following property:

$$R^\alpha(x)[R^\alpha]^\top(x)A \simeq \tilde{A}R^\alpha(x), \quad (27)$$

in which \tilde{A} is an $N \times N$ product operational matrix for the vector A whose elements can be calculated from the below equation by upper property and the orthogonal property Eq. (14):

$$\tilde{a}_{ij} = \frac{j!(j+\alpha)\Gamma^2(\alpha)}{\pi 2^{1-2\alpha}\Gamma(j+2\alpha)} \sum_{k=0}^{N-1} a_k \int_0^\infty R_i^\alpha(x)R_j^\alpha(x)R_k^\alpha(x)w_r^\alpha(x)dx. \quad (28)$$

4 Exponential Gegenbauer functions

We now pay our attention to the exponential Gegenbauer functions which are orthogonal functions on the semi-infinite domain and we introduce them for the first time. The exponential Gegenbauer (E) functions can be defined by $E_n^\alpha(x) = G_n^\alpha(1 - 2e^{-\frac{x}{L}})$, where $\alpha > -\frac{1}{2}$ and the desired interval length is adjusted by parameter L . The recursive formula for these functions are:

$$\begin{cases} E_0^\alpha(x) = 1, \\ E_1^\alpha(x) = 2\alpha(1 - 2e^{-\frac{x}{L}}), \\ E_{n+1}^\alpha(x) = \frac{1}{n+1} [2(1 - 2e^{-\frac{x}{L}})(n+\alpha)E_n^\alpha(x) - (n+2\alpha-1)E_{n-1}^\alpha(x)], n \geq 1. \end{cases} \quad (29)$$

Exponential Gegenbauer functions are also orthogonal on the semi-infinite domain with respect to weighting function $w_e^\alpha(x) = \frac{2}{L}e^{-\frac{x}{L}}[4e^{-\frac{x}{L}}(1 - e^{-\frac{x}{L}})]^{\alpha-\frac{1}{2}}$ and the orthogonality integral equation, similar to Eq. (14) is as follows:

$$\int_0^\infty E_n^\alpha(x)E_m^\alpha(x)w_e^\alpha(x)dx = \frac{\pi 2^{1-2\alpha}\Gamma(n+2\alpha)}{n!(n+\alpha)\Gamma^2(\alpha)}\delta_{nm}, \quad (30)$$

The derivative of the exponential Gegenbauer functions is:

$$\dot{E}_n^\alpha(x) = \frac{d}{dx}E_n^\alpha(x) = \frac{4\alpha}{L}e^{-\frac{x}{L}}E_{n-1}^{\alpha+1}(x). \quad (31)$$

If consider $\widehat{w}_e^\alpha(x) = \frac{L}{8x^2}e^{-\frac{x}{L}}[4e^{-\frac{x}{L}}(1 - e^{-\frac{x}{L}})]^{\alpha+\frac{1}{2}}$ as the weight function of $\dot{E}_n^\alpha(x)$'s functions, then the same quotation in Eq. (17) for the orthogonality property of these functions will be obtained.

Function approximation As mentioned before, to approximate a function on a semi-infinite domain, one can use Eq. (18). In this research, $E_j^\alpha(x)$ is used as basis functions instead of $R_j^\alpha(x)$:

$$\varphi(x) = \sum_{j=0}^\infty a_j E_j^\alpha(x), \quad (32)$$

that

$$a_j = \frac{j!(j+\alpha)\Gamma^2(\alpha)}{\pi 2^{1-2\alpha}\Gamma(j+2\alpha)} \int_0^\infty E_j^\alpha(x)\varphi(x)w_e^\alpha(x)dx. \quad (33)$$

Therefore:

$$\varphi_N(x) = \sum_{j=0}^{N-1} a_j E_j^\alpha(x) = A^T E^\alpha(x), \quad (34)$$

it should be mentioned that the entity of A and $E^\alpha(x)$ vectors are unknown coefficient and exponential Gegenbauer functions with different degrees, respectively:

$$A = [a_0, a_1, \dots, a_{N-1}]^T, \quad (35)$$

$$E^\alpha(x) = [E_0^\alpha(x), E_1^\alpha(x), \dots, E_{N-1}^\alpha(x)]^T. \quad (36)$$

Derivative operational matrix By using a $N \times N$ derivative matrix (D_e) which will be defined later, the following formula for the derivative of the vector $E^\alpha(x)$ will be obtained:

$$\dot{E}^\alpha(x) = \frac{dE^\alpha(x)}{dx} \simeq D_e E^\alpha(x). \quad (37)$$

By deriving each of the expressions in Eq. (29):

$$\begin{cases} \dot{E}_0^\alpha(x) = 0, \\ \dot{E}_1^\alpha(x) = \frac{4\alpha}{L} e^{-\frac{x}{L}} = \frac{1}{L} [2\alpha E_0^\alpha(x) - E_1^\alpha(x)], \\ \dot{E}_{n+1}^\alpha(x) = \frac{1}{n+1} \left[\left(\frac{n}{\alpha} + 1 \right) \frac{d}{dx} (E_n^\alpha(x) \cdot E_1^\alpha(x)) - (n+2\alpha-1) \dot{E}_{n-1}^\alpha(x) \right], n \geq 1. \end{cases} \quad (38)$$

Based on the above equations, a low-triangular matrix is obtained, and $D_e = \frac{\bar{D}_1 + \bar{D}_2}{L}$; where \bar{D}_1 is a diagonal matrix and defined as $D_1 = \text{diag}(-i)$ for $i = 0, \dots, N-1$ and \bar{D}_2 is defined as follow

$$d_{ij} = \begin{cases} 0, & j > i-1, \\ (-1)^{i+j+1} c_{\alpha j}, & j \leq i-1, \end{cases} \quad (39)$$

where $c_{00} = 2$ and otherwise $c_{\alpha j} = 2(\alpha + j)$.

For $N = 5$ and fixed $\alpha \neq 0$ the final matrix will be obtained:

$$D_e = \frac{1}{L} \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 2\alpha & -1 & 0 & 0 & 0 \\ -2\alpha & 2(\alpha+1) & -2 & 0 & 0 \\ 2\alpha & -2(\alpha+1) & 2(\alpha+2) & -3 & 0 \\ -2\alpha & 2(\alpha+1) & -2(\alpha+2) & 2(\alpha+3) & -4 \end{pmatrix}.$$

Also, if we consider $\alpha = 0$ and $L = 1$, the matrix is as follows

$$D_e = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 2 & -1 & 0 & 0 & 0 \\ -2 & 2 & -2 & 0 & 0 \\ 2 & -2 & 4 & -3 & 0 \\ -2 & 2 & -4 & 6 & -4 \end{pmatrix}.$$

As it can be seen, the form of this matrix is simpler than that of the derivation matrix for $R^\alpha(x)$. Consequently, It can be computed faster. In addition, D_e is a lower-triangular matrix but D_r is a lower-Hessenberg matrix, so there exists more zero elements in D_e .

Product operational matrix With considering the production of two exponential Gegenbauer function vectors over a vector A , a matrix \tilde{A} as below:

$$E^\alpha(x) [E^\alpha]^\top(x) A \simeq \tilde{A} E^\alpha(x), \quad (40)$$

The entities \tilde{a}_{ij} of the matrix \tilde{A} can be calculated similar to Eq. (28) except applying exponential functions and related

weights instead of the rational functions and their associated weights:

$$\tilde{a}_{ij} = \frac{j!(j+\alpha)\Gamma^2(\alpha)}{\pi 2^{1-2\alpha}\Gamma(j+2\alpha)} \sum_{k=0}^{N-1} a_k \int_0^\infty E_i^\alpha(x) E_j^\alpha(x) E_k^\alpha(x) w_e^\alpha(x) dx. \quad (41)$$

5 Convergence of the function approximation

In this section an error bound of both rational and exponential Gegenbauer functions approximation are estimated and we show that by increasing N , the approximation solution $\varphi_N(x)$ [Eqs. (20) and (34)] is convergent to $\varphi(x)$ [Eqs. (18) and (32)] exponentially.

Let consider the fixed α and $w(x)$ be $w_r^\alpha(x)$ or $w_e^\alpha(x)$ which are nonnegative, integrable and real-valued weight functions over the interval $I = [0, \infty)$.

Here, we define

$$L_w^2(I) = \{v : I \rightarrow \mathbb{R} \mid v \text{ is measurable and } \|v\|_w < \infty\}, \quad (42)$$

where

$$\|v\|_w = \left(\int_0^\infty v^2(x) w(x) dx \right)^{\frac{1}{2}}, \quad (43)$$

is the norm induced by the scalar product

$$\langle u, v \rangle_w = \int_0^\infty u(x) v(x) w(x) dx. \quad (44)$$

Thus, $\{\psi_j(x)\}_{j \geq 0}$ as $\{R_j^\alpha(x)\}_{j \geq 0}$ or $\{E_j^\alpha(x)\}_{j \geq 0}$ denotes a system which is mutually orthogonal with respect to its weight function w as w_r^α or w_e^α under Eq. (44), i.e.

$$\langle \psi_n, \psi_m \rangle_w = \frac{\pi 2^{1-2\alpha} \Gamma(n+2\alpha)}{n!(n+\alpha)\Gamma^2(\alpha)} \delta_{nm}, \quad (45)$$

and is complete in the space $L_w^2(I)$.

Now, if consider one of the equations of (20) and (34) for approximation of any function $\varphi(x) \in L_w^2(I)$ we can determine the following error:

$$e_N = \|\varphi(x) - \varphi_N(x)\|_w^2. \quad (46)$$

By the completeness of the system $\{\psi_j(x)\}_{j \geq 0}$, when $N \rightarrow \infty$, we have $\varphi_N(x) \rightarrow \varphi(x)$ and $e_N \rightarrow 0$. Furthermore this completeness and definition of $\|\cdot\|_w$ release to rewrite the error in Eq. (46) as

$$\begin{aligned} e_N &= \left\| \sum_{i=N}^{\infty} a_i \psi_i(x) \right\|_w^2 = \sum_{i=N}^{\infty} \sum_{j=N}^{\infty} a_i a_j \langle \psi_i(x), \psi_j(x) \rangle_w \\ &= \sum_{i=N}^{\infty} \sum_{j=N}^{\infty} a_i a_j \frac{\pi 2^{1-2\alpha} \Gamma(i+2\alpha)}{i!(i+\alpha) \Gamma^2(\alpha)} \delta_{ij} \\ &= \sum_{i=N}^{\infty} \frac{\pi 2^{1-2\alpha} \Gamma(i+2\alpha) a_i^2}{i!(i+\alpha) \Gamma^2(\alpha)}, \end{aligned} \quad (47)$$

and according to Eqs. (19) and (33) we have

$$e_N = \sum_{i=N}^{\infty} \frac{i!(i+\alpha) \Gamma^2(\alpha)}{\pi 2^{1-2\alpha} \Gamma(i+2\alpha)} \langle \varphi(x), \psi_i(x) \rangle_w^2. \quad (48)$$

This equation shows that the convergence rate is involved with function $\varphi(x)$. Now, since $\varphi(x) \in L_w^2(I)$, we could present the following theorem about an upper bound for estimating the error of function approximation by $\psi_i(x)$. One Gegenbauer polynomials property which can be helped our proof of the theorem is [68]:

$$x^n = \sum_{0 \leq k \leq n, n-k \equiv 0 \pmod{2}} \frac{(k+\alpha)n! \Gamma(\alpha)}{2^n \left(\frac{n-k}{2}\right)! \Gamma\left(\frac{n+k+2\alpha+2}{2}\right)} G_k^\alpha(x). \quad (49)$$

Theorem 1 Suppose that $\varphi_N(x)$ which is obtained by Eq. (20) or (34) is the best approximation to $\varphi(x) \in L_w^2(I)$ and $\mathcal{F}(y) = \varphi(\Phi(y))$ is analytic on $[-1, 1]$, then an error bound is presented as follows:

$$e_N \leq \sum_{i=N}^{\infty} \frac{\pi 2^{1-2i-2\alpha} \Gamma(i+2\alpha) M_i^2}{(i+\alpha) \Gamma^2(i+\alpha) \Gamma(i+1)} \quad (50)$$

where $\Phi(y) = L\left(\frac{1+y}{1-y}\right)$ or $-L \ln\left(\frac{1-y}{2}\right)$ and $M_i = \max |\mathcal{F}^{(i)}(y)|, y \in (-1, 1)$.

Proof For two cases of $\Phi(y)$ as rational and exponential mapping, we have the following properties:

Rational mapping

$$\begin{cases} \Phi(y) = L\left(\frac{1+y}{1-y}\right), & R_n^\alpha(\Phi(y)) = G_n^\alpha(y), \\ w_r^\alpha(\Phi(y)) = \frac{(1-y)^2}{2L} (1-y^2)^{\alpha-\frac{1}{2}}, & dx = \frac{2L}{(1-y)^2} dy. \end{cases}$$

Exponential mapping

$$\begin{cases} \Phi(y) = -L \ln\left(\frac{1-y}{2}\right), & E_n^\alpha(\Phi(y)) = G_n^\alpha(y), \\ w_e^\alpha(\Phi(y)) = \frac{1-y}{L} (1-y^2)^{\alpha-\frac{1}{2}}, & dx = \frac{L}{1-y} dy. \end{cases}$$

Now, if consider each case in $\langle \varphi(x), \psi_i(x) \rangle_w$ we have:

$$\langle \varphi(x), \psi_i(x) \rangle_w = \int_{-1}^1 \mathcal{F}(y) G_i^\alpha(y) w(y) dy. \quad (51)$$

Since $\mathcal{F}(y)$ is analytical, can have the Taylor's formula for $i \geq N$ as follow:

$$\begin{aligned} \langle \varphi(x), \psi_i(x) \rangle_w &= \sum_{h=0}^{i-1} \frac{\mathcal{F}^{(h)}(0)}{h!} \int_{-1}^1 y^h G_i^\alpha(y) w(y) dy \\ &+ \frac{\mathcal{F}^{(i)}(\xi_i)}{i!} \int_{-1}^1 y^i G_i^\alpha(y) w(y) dy, \quad \xi_i \in (-1, 1). \end{aligned}$$

According to Eq. (49) and because of the orthogonality of the basis functions,

$$\int_{-1}^1 y^h G_i^\alpha(y) w(y) dy = 0, \quad h = 0, 1, \dots, i-1, \quad (52)$$

and the remaining phrase respect to Eq. (49), can be rewritten as the following:

$$\begin{aligned} \langle \varphi(x), \psi_i(x) \rangle_w &= \frac{\mathcal{F}^{(i)}(\xi_i)}{i!} \frac{\pi i! 2^{1-2\alpha} \Gamma(i+2\alpha)}{i! 2^i \Gamma(\alpha) \Gamma(i+1+\alpha)} \\ &\leq \frac{\pi 2^{1-2\alpha} \Gamma(i+2\alpha) M_i}{i! 2^i \Gamma(\alpha) \Gamma(i+1+\alpha)}. \end{aligned} \quad (53)$$

So, by substituting above inequality in Eq. (48), the proof is completed. \square

This theorem demonstrates that any function defined in $L_w^2(I)$, which their rational and exponential mapping are analytic, has a series solution in the forms Eqs. (20) and (34), respectively, with the exponential convergence.

6 RGT and EGT method for solving the problem

In this part, the proposed functions in Tau method was implemented to the rational Gegenbaure Tau (RGT) and the exponential Gegenbaure Tau (EGT) methods to solve Eq. (6). After choosing a value for α parameter, and considering $\psi(\eta) = R^\alpha(\eta)$ in the following formulas to solve the problem. Then assume $\psi(\eta) = E^\alpha(\eta)$ and apply EGT method. For comparison the obtained results are compared with RGT and EGT methods. The three functions in Eq. (6) and their derivatives are as follows:

$$f(\eta) \simeq f_N(\eta), \quad (54)$$

$$f_N(\eta) = \sum_{i=0}^{N-1} a_i \psi_i(\eta) = A^T \psi(\eta), \quad (55)$$

$$f_N^{(j)}(\eta) = \sum_{i=0}^{N-1} a_i \psi_i^{(j)}(\eta) \simeq A^T D^j \psi(\eta) \quad j = 1, 2, 3, \quad (56)$$

$$g(\eta) \simeq g_N(\eta), \quad (57)$$

$$g_N(\eta) = \sum_{i=0}^{N-1} b_i \psi_i(\eta) = B^T \psi(\eta), \quad (58)$$

$$g_N^{(j)}(\eta) = \sum_{i=0}^{N-1} b_i \psi_i^{(j)}(\eta) \simeq B^T D^j \psi(\eta) \quad j = 1, 2, \quad (59)$$

$$\theta(\eta) \simeq \theta_N(\eta), \quad (60)$$

$$\theta_N(\eta) = \sum_{i=0}^{N-1} c_i \psi_i(\eta) = C^T \psi(\eta), \quad (61)$$

$$\theta_N^{(j)}(\eta) = \sum_{i=0}^{N-1} c_i \psi_i^{(j)}(\eta) \simeq C^T D^j \psi(\eta) \quad j = 1, 2, \quad (62)$$

where D^j is obtained by multiplying it by itself j -times and it can be D_r or D_e given in Eqs. (23) or (37). By using above equations, then

$$f_N(\eta) f_N''(\eta) \simeq A^T \psi(\eta) \psi^T(\eta) (D^2)^T A \\ = A^T \psi(\eta) \psi^T(\eta) U \simeq A^T \tilde{U} \psi(\eta), \quad (63)$$

$$f_N'^2(\eta) \simeq A^T D \psi(\eta) \psi^T(\eta) D^T A \\ = A^T D \psi(\eta) \psi^T(\eta) V \simeq A^T D \tilde{V} \psi(\eta), \quad (64)$$

$$f_N''^2(\eta) \simeq A^T D^2 \psi(\eta) \psi^T(\eta) (D^2)^T A \\ = A^T D^2 \psi(\eta) \psi^T(\eta) U \simeq A^T D^2 \tilde{U} \psi(\eta), \quad (65)$$

$$f_N(\eta) \theta_N'(\eta) \simeq A^T \psi(\eta) \psi^T(\eta) D^T C \\ = A^T \psi(\eta) \psi^T(\eta) W \simeq A^T \tilde{W} \psi(\eta), \quad (66)$$

$$f_N'(\eta) \theta_N(\eta) \simeq A^T D \psi(\eta) \psi^T(\eta) C \\ \simeq A^T D \tilde{C} \psi(\eta), \quad (67)$$

where $U = (D^2)^T A$, $V = D^T A$, $W = D^T C$ and the elements of matrices \tilde{U} , \tilde{V} , \tilde{W} and \tilde{C} , can be calculated similar to Eqs. (28) and (41).

Now, consider the three equation in Eq. (6), the following residual functions ($\text{Res}_1(\eta)$, $\text{Res}_2(\eta)$, $\text{Res}_3(\eta)$) can be considered:

$$\text{Res}_1(\eta) = [A^T D^3 + A^T \tilde{U} - A^T D \tilde{V} - M A^T D \\ + K B^T D] \psi(\eta), \quad (68)$$

$$\text{Res}_2(\eta) = [G B^T D^2 - (2 B^T + A^T D^2)] \psi(\eta), \quad (69)$$

$$\text{Res}_3(\eta) = \left[\left(\frac{1+R}{R \text{Pr}} \right) C^T D^2 + A^T \tilde{W} - \gamma A^T D \tilde{C} \right. \\ \left. + \text{Ec} (A^T D^2 \tilde{U}) \right] \psi(\eta). \quad (70)$$

Now, by applying the Tau method [1, 6, 22], $3(N-2)$ algebraic equations by the following equations will be obtained:

$$\langle \text{Res}_1(\eta), \psi_k(\eta) \rangle \\ = \int_0^\infty \text{Res}_1(\eta) \psi_k(\eta) w(\eta) d\eta = 0, \quad k = 0, 1, \dots, N-3, \quad (71)$$

$$\langle \text{Res}_2(\eta), \psi_k(\eta) \rangle \\ = \int_0^\infty \text{Res}_2(\eta) \psi_k(\eta) w(\eta) d\eta = 0, \quad k = 0, 1, \dots, N-3, \quad (72)$$

$$\langle \text{Res}_3(\eta), \psi_k(\eta) \rangle \\ = \int_0^\infty \text{Res}_3(\eta) \psi_k(\eta) w(\eta) d\eta = 0, \quad k = 0, 1, \dots, N-3, \quad (73)$$

Note that $w(\eta)$ in the above equations, is the weight function and can be chosen as $w_r^x(\eta)$ or $w_e^x(\eta)$ according to the selected method.

With implementing the boundary conditions:

$$f_N(0) \\ = A^T \psi(0) = f_w, \quad f_N'(0) = A^T D \psi(0) = 1, \quad (74)$$

$$g_N(0) \\ = B^T \psi(0) = 0, \quad \lim_{\eta \rightarrow \infty} g_N(\eta) \\ = \lim_{\eta \rightarrow \infty} B^T \psi(\eta) = 0, \quad (75)$$

$$\theta_N(0) \\ = C^T \psi(0) = 1, \quad \lim_{\eta \rightarrow \infty} \theta_N(\eta) \\ = \lim_{\eta \rightarrow \infty} C^T \psi(\eta) = 0, \quad (76)$$

and another boundary condition ($f'(\infty) = 0$) is already satisfied.

Among to Eqs. (71)–(76), a system of nonlinear equations with $3N$ equations and $3N$ unknown coefficients include a_i , b_i and c_i of the vector A , B and C in Eqs. (55), (58) and (61) are obtained which can be calculated.

Table 1 The residual functions for three equations in main problem by using RGT and EGT methods with various α and N , when $M = 2, K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2$ and $Ec = 0.02$

α	N	RGT			EGT		
		$\ Res_1\ ^2$	$\ Res_2\ ^2$	$\ Res_3\ ^2$	$\ Res_1\ ^2$	$\ Res_2\ ^2$	$\ Res_3\ ^2$
-0.4	5	1.82E-02	6.84E-02	6.52E-03	5.57E-02	4.19E-02	6.69E-02
	7	9.59E-03	3.86E-03	1.67E-02	2.38E-06	4.16E-08	2.22E-03
	11	2.38E-04	6.18E-06	4.43E-05	3.08E-11	9.28E-10	6.67E-06
	15	7.71E-08	6.31E-08	2.21E-07	5.71E-14	1.21E-10	8.42E-09
0	5	1.51E-02	6.54E-02	5.49E-03	2.98E-02	2.22E-02	2.83E-02
	7	1.55E-02	4.86E-03	8.03E-03	1.36E-06	4.74E-08	9.14E-04
	11	1.07E-04	6.03E-06	1.48E-05	2.10E-11	5.43E-11	3.27E-06
	15	4.94E-08	1.57E-08	1.45E-07	2.21E-17	8.99E-14	3.94E-09
0.5	5	5.98E-02	1.07E-01	4.13E-03	2.28E-02	1.65E-02	1.66E-02
	7	2.51E-02	7.42E-03	3.55E-03	1.04E-06	5.95E-08	5.26E-04
	11	5.36E-04	1.99E-05	2.55E-05	1.73E-11	6.51E-11	4.25E-06
	15	5.90E-08	5.10E-08	1.87E-07	4.55E-14	9.93E-11	5.19E-09
1.5	5	9.99E-02	1.46E-01	2.32E-03	2.96E-02	1.97E-02	1.37E-02
	7	4.94E-02	1.66E-02	4.12E-03	2.11E-06	1.76E-07	8.53E-04
	11	1.94E-03	9.29E-05	5.13E-05	5.39E-11	4.51E-10	6.50E-06
	15	1.69E-07	5.32E-07	2.01E-07	6.31E-12	7.95E-10	2.03E-08
2.5	5	1.24E-01	1.77E-01	1.50E-03	4.25E-02	2.69E-02	1.62E-02
	7	7.80E-02	3.14E-02	6.65E-03	4.86E-06	5.15E-07	1.39E-03
	11	5.14E-03	2.97E-04	3.27E-04	2.37E-10	1.32E-11	1.82E-05
	15	1.88E-05	4.08E-06	3.49E-06	1.29E-12	7.04E-10	8.14E-08
3.5	5	1.38E-01	2.02E-01	1.20E-03	5.50E-02	3.40E-02	1.93E-02
	7	1.08E-01	5.26E-02	7.91E-03	8.59E-06	1.12E-06	1.70E-03
	11	1.12E-02	7.22E-04	1.08E-03	7.12E-10	7.27E-11	2.30E-05
	15	6.34E-05	1.94E-05	2.35E-05	1.45E-12	3.70E-11	1.59E-07

7 Numerical results and discussions

In this section, we first solve the special case of the studied problem when $M = 2, K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2$ and $Ec = 0.02$ by RGT and EGT method with various α such as $-0.4, 0, 0.5, 1.5, 2.5$ and 3.5 and reporting the residual functions for different N in Table 1 while selecting $L = 4$ as the scaling factor. The residual functions by using Eq. (6) can be written as:

$$\begin{aligned}
 Res_1(\eta) &= f_N'''(\eta) + f_N(\eta)f_N''(\eta) - (f_N'(\eta))^2 \\
 &\quad - Mf_N'(\eta) + Kg_N'(\eta), \\
 Res_2(\eta) &= Gg_N''(\eta) - (2g_N(\eta) + f_N''), \\
 Res_3(\eta) &= \left(\frac{1+R}{RPr}\right)\theta_N''(\eta) + f_N(\eta)\theta_N'(\eta) \\
 &\quad - \mathcal{W}f_N'(\eta)\theta_N(\eta) + Ec(f_N''(\eta))^2,
 \end{aligned} \tag{77}$$

and calculate $\|Res\|^2$ by means of

$$\|Res\|^2 = \int_0^\infty Res^2(\eta) d\eta. \tag{78}$$

According to this table, the downward trend of values of $\|Res_1\|^2$, $\|Res_2\|^2$ and $\|Res_3\|^2$ by increasing N , indicates

the fast convergence and good accuracy of the method for all cases of reported α . By investigation of the obtained values, it seems that the best interval for α is $(-0.5, 0.5]$ which $\alpha = 0$ has the better results. Based on this table and the absolute coefficients $|a_i|$, $|b_i|$ and $|c_i|$ of two categories of rational and exponential Gegenbauer functions are shown in Figs. 1, 2 and 3, it can be concluded that accurate solutions can be obtained by the implemented method even with small $N = 15$. So, we solve the rest of the cases of the problem by these parameters ($N = 15, \alpha = 0$ and $L = 4$) and report the residual values of the rational and the exponential Gegenbauer Tau method in Table 2.

The results in tables at expressed points $(f''(0), g'(0), \theta'(0))$ will be presented to investigate the behaviour of them for various parameters and compare them with the result of analytical (successive approximation) and numerical (shooting method) methods which reported in [57]. We know that $-f''(0)$, $g'(0)$ and $-\theta'(0)$ are the skin friction coefficient at the wall, wall couple stress and the local Nusselt number, respectively. So, we show the influences of parameter coupling constant on these criterions in Table 3. The two parameters that are

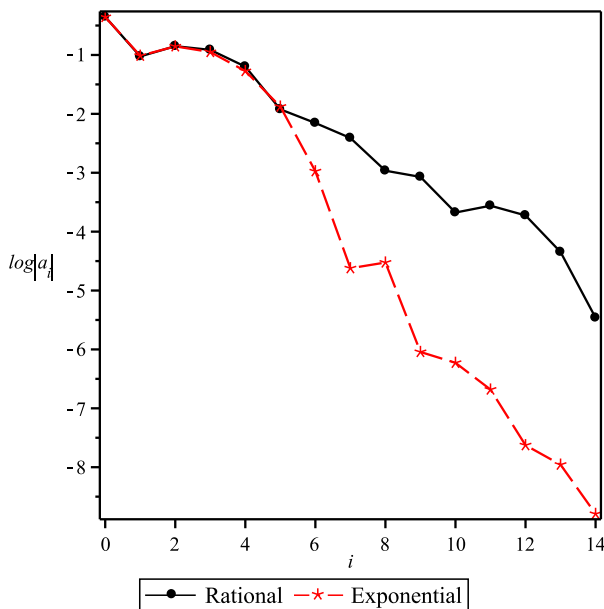


Fig. 1 Comparison between absolute coefficients $|a_i|$ of two categories of rational and exponential Gegenbauer functions when $M = 2, K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

directly related to the coupling rate are $-\theta'(0)$ and $g'(0)$, but the value of $-f''(0)$ is inversely related to the coupling rate.

Tables 4, 5 and 6 show that among the magnetic field, Prandtl number and radiation parameter, only the magnetic field affects the parameters of skin friction coefficient and wall couple stress whose values are increased by increasing the level of the magnetic field. This is expected since the linear and angular momentum equations [the first and the second equations in Eq. (6)] are uncoupled from the energy equation [the third equation in Eq. (6)] for this problem. Moreover, although increasing the Prandtl number and radiation parameter cause to increase the local Nusselt number, but this parameter decreases by the presence of the magnetic field.

The influence of the mass transfer parameter (f_w) is presented in Table 7. It shows that injection ($f_w \leq 0$) reduces all three parameters mentioned above, but suction ($f_w > 0$) increases them.

By considering obtained results in previous tables and figures, it is concluded that accuracy and convergency of EGT method is better for solving this problem. Also CPU time of solving the Eqs. (71)–(76) for RGT and EGT methods in Maple 18 software on a PC, CPU 2.2 GHz are presented in Table 8. With comparing the results it is concluded that EGT method is faster than RGT method for solving the problem. Therefore, for obtaining more results, EGT method was implemented.

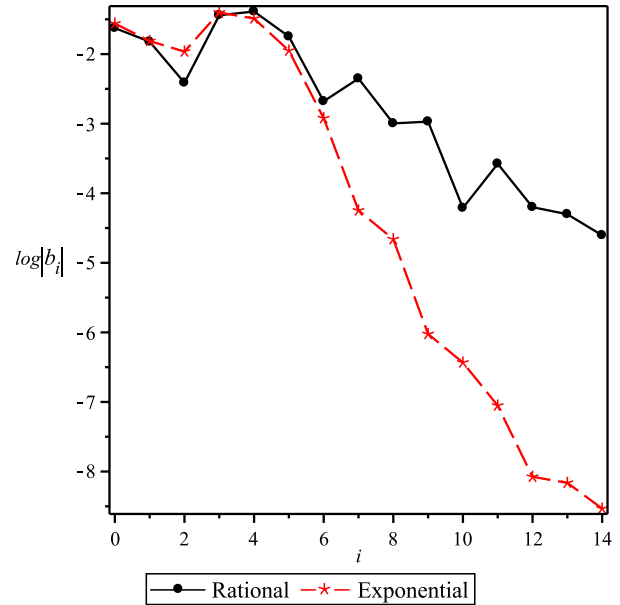


Fig. 2 Comparison between absolute coefficients $|b_i|$ of two categories of rational and exponential Gegenbauer functions when $M = 2, K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

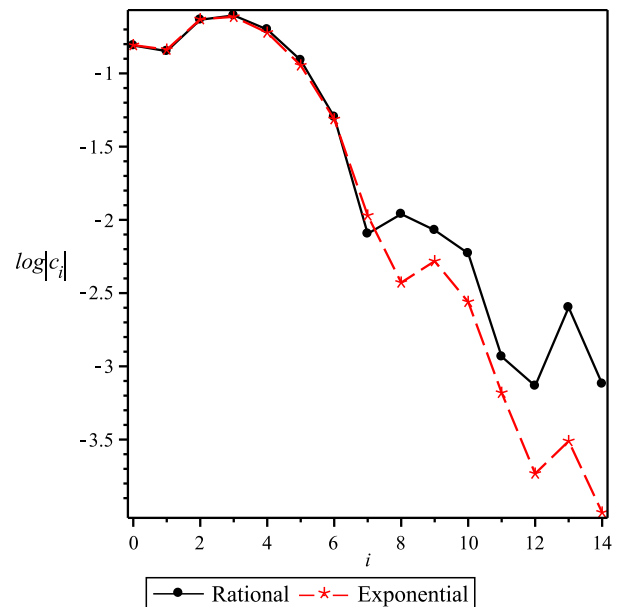


Fig. 3 Comparison between absolute coefficients $|c_i|$ of two categories of rational and exponential Gegenbauer functions when $M = 2, K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

In Figs. 4 and 5 the effect of the coupling parameter is considered and they show that by increasing K , $f'(\eta)$ decrease and $g(\eta)$ increases. Note that the velocity boundary layer thickness increased with increasing values

Table 2 The residual functions for three equations in main problem by using RGT and EGT methods when $\alpha = 0$ and $N = 15$

K	M	Pr	R	f_w	G	γ	Ec	RGT			EGT		
								$\ \text{Res}_1\ ^2$	$\ \text{Res}_2\ ^2$	$\ \text{Res}_3\ ^2$	$\ \text{Res}_1\ ^2$	$\ \text{Res}_2\ ^2$	$\ \text{Res}_3\ ^2$
1	2	10	3	0	2	1	0.02	5.94E-08	1.57E-08	1.87E-07	2.21E-17	8.99E-14	6.94E-09
4	2	10	3	0	2	1	0.02	3.95E-04	1.73E-06	1.93E-07	6.34E-10	4.26E-11	8.67E-09
1	1	10	3	0	2	1	0.02	9.25E-05	3.12E-07	7.89E-07	7.71E-13	5.32E-14	4.11E-08
1	3.8	10	3	0	2	1	0.02	2.32E-07	5.34E-10	1.64E-08	2.56E-16	4.10E-15	3.86E-10
1	2	0.71	3	0	2	1	0.02	5.94E-08	1.57E-08	1.93E-07	2.22E-17	7.26E-15	1.67E-07
1	2	5	3	0	2	1	0.02	5.94E-08	1.57E-08	4.58E-11	2.22E-17	7.26E-15	1.73E-11
1	2	10	0.1	0	2	1	0.02	5.94E-08	1.57E-08	1.00E-08	2.22E-17	7.26E-15	1.08E-13
1	2	10	0.5	0	2	1	0.02	5.94E-08	1.57E-08	3.91E-11	2.22E-17	7.26E-15	3.45E-12
1	2	10	1	0	2	1	0.02	5.94E-08	1.57E-08	4.11E-09	2.22E-17	7.26E-15	4.82E-10
1	2	10	3	-0.5	2	1	0.02	3.94E-05	2.33E-07	7.50E-10	2.82E-08	7.08E-12	3.27E-12
1	2	10	3	0.5	2	1	0.02	6.54E-06	1.63E-08	1.64E-06	2.46E-08	4.93E-12	3.86E-07

Table 3 Comparison between RGT and EGT methods with results of [57] for $f''(0)$, $g'(0)$ and $\theta'(0)$ by various K when $M = 2, f_w = 0, \text{Pr} = 10, R = 3, \gamma = 1, G = 2, \text{Ec} = 0.02$

K	Analytical [57]	Numerical [57]	RGT	EGT
$f''(0)$				
1	-1.676622	-1.676305	-1.676350	-1.676305
4	-1.493959	-1.494670	-1.498385	-1.494670
$g'(0)$				
1	0.310602	0.317949	0.317946	0.317949
4	0.325028	0.321999	0.321966	0.321999
$\theta'(0)$				
1	-2.933228	-2.932841	-2.928977	-2.932825
4	-2.973965	-2.974663	-2.960146	-2.965177

Table 4 Comparison between RGT and EGT methods with results of [57] for $f''(0)$, $g'(0)$ and $\theta'(0)$ by various M when $K = 1, f_w = 0, \text{Pr} = 10, R = 3, \gamma = 1, G = 2, \text{Ec} = 0.02$

M	Analytical [57]	Numerical [57]	RGT	EGT
$f''(0)$				
1	-1.358082	-1.358217	-1.360011	-1.358217
2	-1.676622	-1.676305	-1.676350	-1.676305
3.8	-2.138957	-2.138018	-2.137928	-2.138018
$g'(0)$				
1	0.283562	0.294877	0.294868	0.294877
2	0.310602	0.317949	0.317946	0.317949
3.8	0.339333	0.343713	0.343713	0.343713
$\theta'(0)$				
1	-3.033721	-3.034414	-3.027976	-3.034371
2	-2.933228	-2.932841	-2.928977	-2.932825
3.8	-2.779171	-2.779855	-2.779873	-2.781256

Table 5 Comparison between RGT and EGT methods with results of [57] for $f''(0)$, $g'(0)$ and $\theta'(0)$ by various Pr when $M = 2, K = 1, f_w = 0, R = 3, \gamma = 1, G = 2, \text{Ec} = 0.02$

Pr	Analytical [57]	Numerical [57]	RGT	EGT
$f''(0)$				
0.71	-1.676622	-1.676305	-1.676350	-1.676305
5	-1.676622	-1.676305	-1.676350	-1.676305
10	-1.676622	-1.676305	-1.676350	-1.676305
$g'(0)$				
0.71	0.310602	0.317949	0.317946	0.317949
5	0.310602	0.317949	0.317946	0.317949
10	0.310602	0.317949	0.317946	0.317949
$\theta'(0)$				
0.71	-0.507583	-0.500570	-0.478292	-0.478260
5	-1.948456	-1.949998	-1.949977	-1.949998
10	-2.933228	-2.932841	-2.928977	-2.932825

of K associated with the decrease in the wall velocity gradient. The relationship between the coupling parameter and the temperature profile is straightforward, but due to the slight increase in $\theta(\eta)$ with increasing coupling, we have not drawn its figure. The desired functions (fluid velocity, angular-velocity and temperature profile) are influenced by the magnetic field whose figures are shown in Figs. 6, 7 and 8, respectively. With the presence of a magnetic field, the flow face to a drag-like force, namely the Lorentz force whose action is opposite to the direction of the fluid motion and causes to decreasing the fluid velocity and angular-velocity but instead increasing the fluid temperature. The velocity boundary layer thickness decreases while the thermal boundary layer thickness increases as M increases. In addition, the maximum of the

Table 6 Comparison between RGT and EGT methods with results of [57] for $f''(0)$, $g'(0)$ and $\theta'(0)$ by various R when $M = 2$, $K = 1$, $f_w = 0$, $Pr = 10$, $\gamma = 1$, $G = 2$, $Ec = 0.02$

R	Analytical [57]	Numerical [57]	RGT	EGT
$f''(0)$				
0.1	-1.676622	-1.676305	-1.676350	-1.676305
0.5	-1.676622	-1.676305	-1.676350	-1.676305
1	-1.676622	-1.676305	-1.676350	-1.676305
3	-1.676622	-1.676305	-1.676350	-1.676305
$g'(0)$				
0.1	0.310602	0.317949	0.317946	0.317949
0.5	0.310602	0.317949	0.317946	0.317949
1	0.310602	0.317949	0.317946	0.317949
3	0.310602	0.317949	0.317946	0.317949
$\theta'(0)$				
0.1	-0.719536	-0.742685	-0.737100	-0.737100
0.5	-1.807747	-1.813284	-1.813271	-1.813283
1	-2.317869	-2.318467	-2.318089	-2.318462
3	-2.933228	-2.932841	-2.928977	-2.932825

angular velocity decreases in amplitude and the location of the maximum velocity moves closer to the wall with an increase of M . According to the tables, the Prandtl number and radiation parameter just effects with inversely related on temperature profile $\theta(\eta)$, Figs. 9 and 10, respectively. As the Prandtl increases, there is a fall in the fluid temperature as well as its boundary layer thickness. This causes the wall slope of the temperature profile to decrease as Pr increases, causing the Nusselt number to increase as clearly was shown in Table 5. It should be noted that when $R \rightarrow \infty$, we are facing a condition where thermal radiation effect is absent. This indicates that as the parameter R

Table 8 The computer run time of RGT and EGT methods in second when $N = 15$

K	M	Pr	R	f_w	G	γ	Ec	RGT (s)	EGT (s)
1	2	10	3	0	2	1	0.02	2.293	1.408
4	2	10	3	0	2	1	0.02	2.543	1.482
1	1	10	3	0	2	1	0.02	2.580	1.482
1	3.8	10	3	0	2	1	0.02	1.638	1.436
1	2	0.71	3	0	2	1	0.02	2.231	1.778
1	2	5	3	0	2	1	0.02	2.481	1.950
1	2	10	0.1	0	2	1	0.02	2.652	2.059
1	2	10	0.5	0	2	1	0.02	2.636	2.106
1	2	10	1	0	2	1	0.02	2.605	2.091
1	2	10	3	-0.5	2	1	0.02	2.371	1.966
1	2	10	3	0.5	2	1	0.02	3.136	2.858

increases, thermal radiation effects become lower and this means that the temperature decreases and the negative slope of the temperature profile at the surface increases as shown in Table 5. At last, different mass transfer f_w considered and the effect of this parameter on three desired profiles as $f'(\eta)$, $g(\eta)$ and $\theta(\eta)$ and illustrated in Figs. 11, 12 and 13, respectively, which show that suction leads to decrease all profiles and injection leading to opposite behaviour. Applying suction at the stretching surface causes to draw the amount of the fluid into the surface and consequently the hydrodynamic boundary layer thickness decreases. If ($f_w > 0$), high resistance afford by the fluid and has a tendency to reduce the velocity of the flow, but wall injection ($f_w \leq 0$) produces the opposite effect. Also, the thermal boundary layer gets depressed by increasing the suction parameter. Therefore, for increasing the value of f_w , the temperature field gradually decreases.

Table 7 Comparison between RGT and EGT methods with results of [57] for $f''(0)$, $g'(0)$ and $\theta'(0)$ by various f_w when $M = 2$, $K = 1$, $Pr = 10$, $R = 3$, $\gamma = 1$, $G = 2$, $Ec = 0.02$

f_w	Analytical [57]	Numerical [57]	RGT	EGT
$f''(0)$				
-0.5	-1.434341	-1.444333	-1.445684	-1.444294
0	-1.676622	-1.676305	-1.676350	-1.676305
0.5	-1.940262	-1.946052	-1.945493	-1.946015
$g'(0)$				
-0.5	0.292893	0.300334	0.300312	0.300334
0	0.310602	0.317949	0.317946	0.317949
0.5	0.327805	0.334831	0.334828	0.334831
$\theta'(0)$				
-0.5	-1.398473	-1.392094	-1.392090	-1.392087
0	-2.933228	-2.932841	-2.928977	-2.932825
0.5	-5.528042	-5.527730	-5.558338	-5.526077

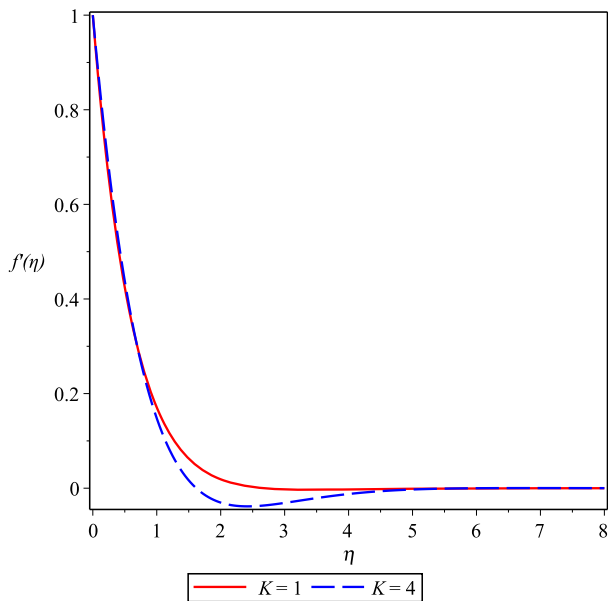


Fig. 4 Velocity profile-dependence of coupling constant parameter K , when $M = 2, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

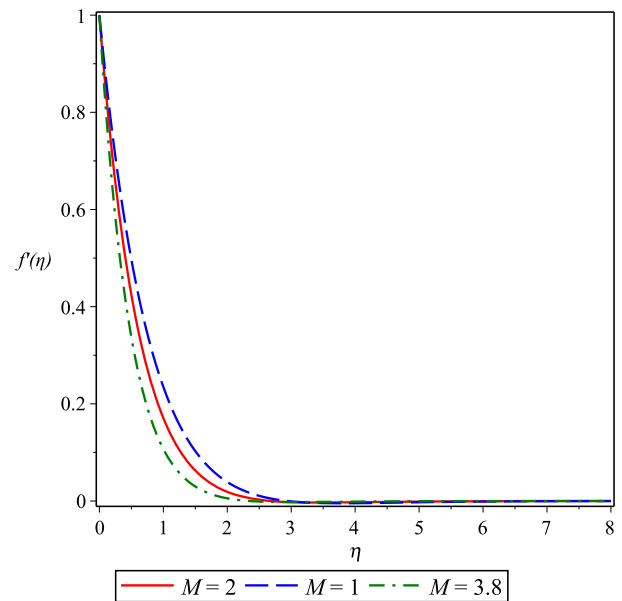


Fig. 6 Velocity profile-dependence of magnetic parameter M , when $K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

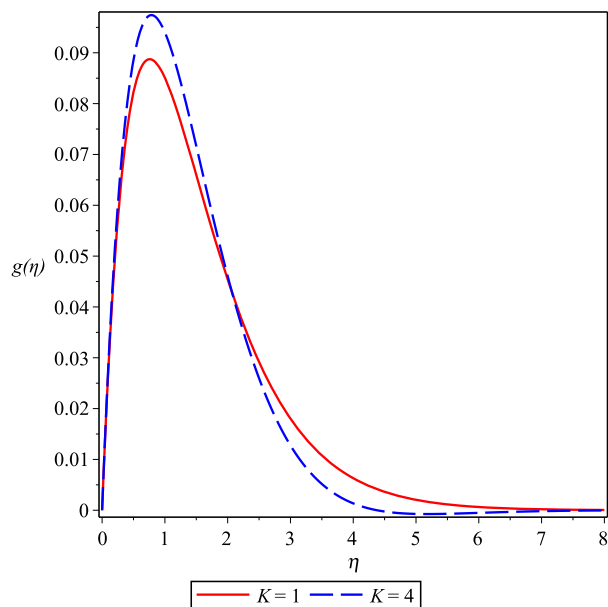


Fig. 5 Angular velocity profile-dependence of coupling constant parameter K , when $M = 2, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

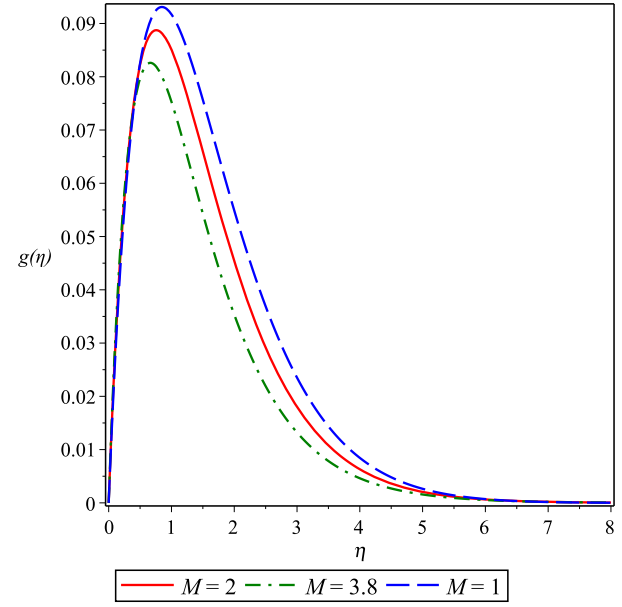


Fig. 7 Angular Velocity profile-dependence of magnetic parameter M , when $K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

8 Conclusions

In this paper, a numerical approach called Tau method has been implemented to solve the system of coupled nonlinear ordinary differential equations. The fluid flow consists a MHD micropolar fluid which past a moving plate with

suction and injection boundary conditions with considering heat transfer. In this research, two different functions were used; rational and exponential Gegenbauer functions. For solving the system of equations basis functions of Tau method was implemented. To the best of our knowledge, this is the first time that the derivative matrices of these functions were introduced and applied to Tau method for

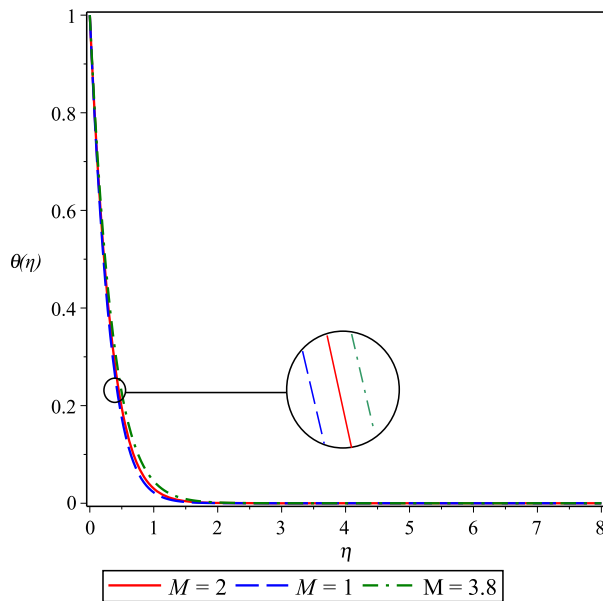


Fig. 8 Temperature profile-dependence of magnetic parameter M , when $K = 1, f_w = 0, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

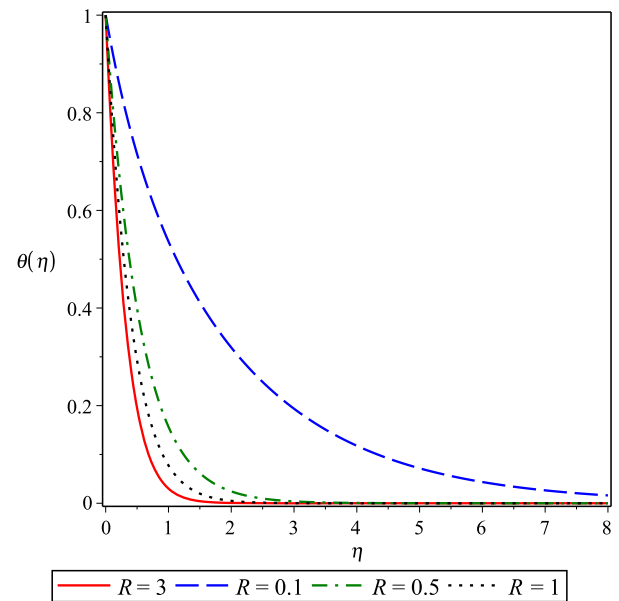


Fig. 10 Temperature profile-dependence of radiation parameter R , when $M = 2, K = 1, f_w = 0, Pr = 10, \gamma = 1, G = 2, Ec = 0.02$

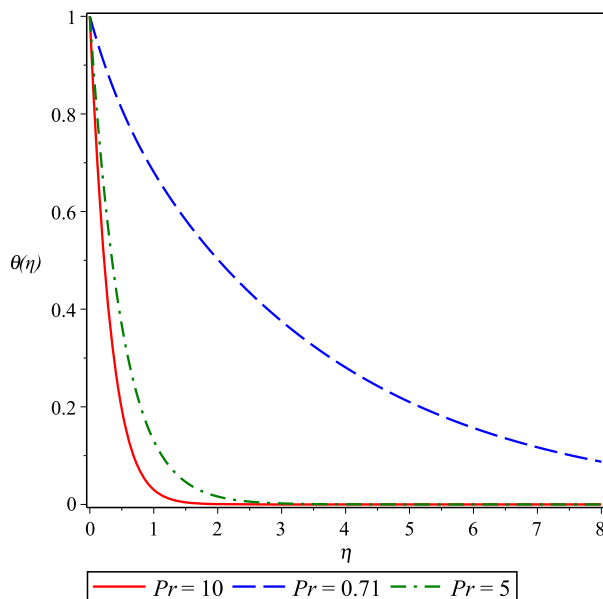


Fig. 9 Temperature profile-dependence of Prandtl number Pr , when $M = 2, K = 1, f_w = 0, R = 3, \gamma = 1, G = 2, Ec = 0.02$

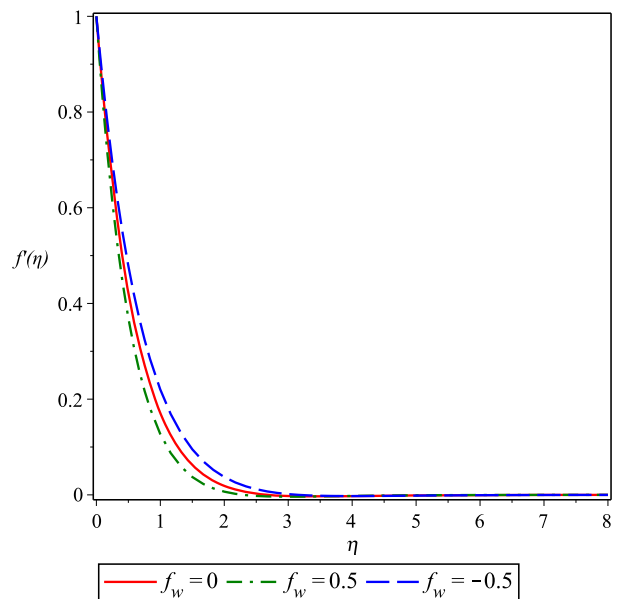


Fig. 11 Velocity profile-dependence of mass transfer parameter f_w , when $M = 2, K = 1, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

solving a complicated heat and mass transfer phenomena. Also, the exponential convergence rate of approximation of the analytical functions by these basis functions was discussed in this paper. In the numerical result section, the effects of some important physical parameters of the system were discussed through tables and graphs. According

to the good stability and convergence rate of Tau method, it can be used for solving similar problem, also it should be mentioned that the considered computational domain is infinite and this proves that this method has a good ability for solving boundary layer problems, such as the solved problem by considering the induced magnetic field and the

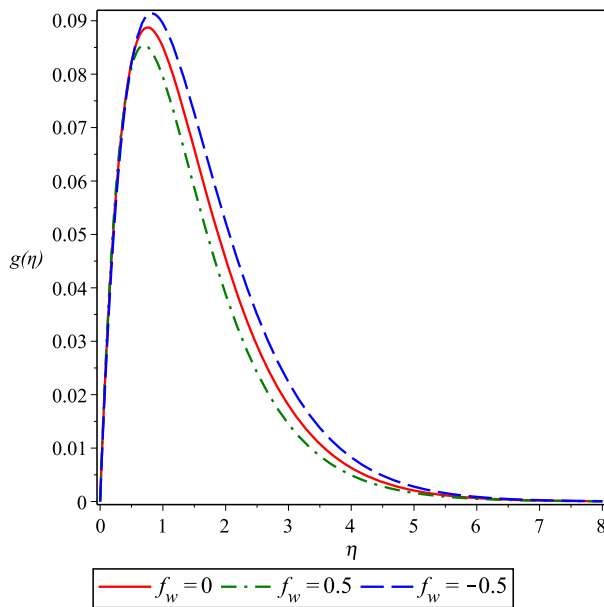


Fig. 12 Angular velocity profile-dependence of mass transfer parameter f_w , when $M = 2, K = 1, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

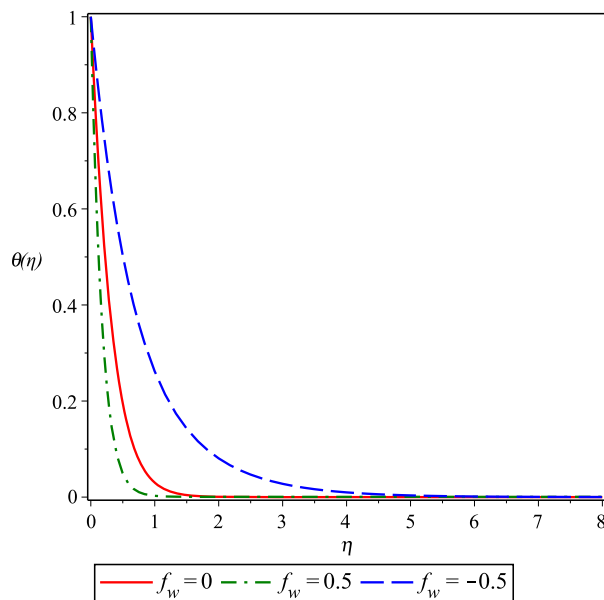


Fig. 13 Temperature profile-dependence of mass transfer parameter f_w , when $M = 2, K = 1, Pr = 10, R = 3, \gamma = 1, G = 2, Ec = 0.02$

Hall effect are included. The obtained results have excellent agreement with the approximate and exact solution. Although both introduced basis functions have provided an acceptable result for this equation in Tau method, according to the residual functions, it seems that the accuracy and speed convergence of the exponential Gegenbauer Tau method is much better for solving this problem. At last, we

note that the introduced methods can be applied even for the PDEs system as well as fractional PDEs by expanding the multi-variable functions and using the operational matrices to obtain partial derivatives and the residual functions.

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